

A Two-Stage Taguchi Design Example—Image Quality Promotion in Miniature Camera/Cell-Phone Lens

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Abstract

A simple, practical manufacturing process, integrating manufacturing capability-oriented design (MCOD) philosophy and Taguchi's method, is presented to tackle the high resolution miniature camera/cell phone lens issues at the manufacturing phase. Meanwhile, we also use optical software to create an analytical simulation model to investigate the quality characteristics due to lens' thickness, eccentricity, surface profile, and air lens' gap; a single quality characteristics expressed in terms of modulation transfer function (MTF) is defined. Optimal combination of process parameters in experimental scenario using Taguchi's method is performed, and the results are judged and analyzed by the indices of signal-to-noise ratio (S/N) and the analysis of variance (ANOVA). The key idea of the two-stage design is to utilize optical software to conduct the sensitivity analysis of MTF first; an analytical model, dependent on actual process parameters at manufacturing stage, is constructed next; and finally by substituting these outputs from the analytical model back to the optical software to verify the design criterion and do the modifications. By minimizing both the theoretical errors at design stage and the complexity in the manufacturing process, we are able to seeking for the most economical solution, simultaneously attain the optimal/suboptimal combination of process parameters or control factors in lens manufacturing issue.

Keywords: Taguchi Method, MTF, Lens

1. Introduction

Taguchi method [1-2] basically focuses on the design of experiments, determining the couplings between the quality characteristics (output) and the control factors (input), possessing a certain number of levels. Taguchi method has been popular in the fields of optical and lens designs/manufacturing. Use of both Taguchi method and principle component analysis (PCA) to achieve multiple performance characteristics (MPC) (or multi-objective) for a U-type 2X zoom projection lens set was presented in section 3. The system complexity was increasing, and the SPSS software was employed to generate the outputs with the corresponding given inputs, i.e., the training procedure is unavoidable and necessary for obtaining principle components. By combining fuzzy-logic with Taguchi method, a successful simulation was claimed, that is, eliminating primary aberrations for U-type 2X zoom optics with freeform surface.[3-4]

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A new concept for the optimization and optical design[5] of miniature digital zoom optics with liquid lens elements is proposed in this research. It propose a newly developed digital zoom layout and optimization with a modified genetic algorithm (GA) method, in order to meet the demands of a certain specification. The results show that achieve a successful optical design and the optimization of the digital zoom optics with liquid optics, whose performance is greatly improved up to 48.68%, from the standpoint of onaxis spot size. From the photographer point of view, contrast and resolution are nevertheless in conflict. One fair index for the quality analysis in photorgraphy is the modulation trasfer function (MTF), describing the complex interaction between resolution and contrast. Eventually, MTF is adopted to be the quality characteristics here.

The ultimate goal of our design is to design an simple, alternative manufacturing process for lens manufacturing to accelerate the time-to-market instead of using the aforementioned methods with high system complexity in software, hardware, or manufacturing processes. In this analysis, an orthogonal array, consisting of a number of 18 experiments, 8 control factors with each maintaining 3 levels except the first one, which is only containing 2 levels, is constructed to enhance the quality characteristics, MTF, in our case. Interaction issue is hereafter not discussed and neglected herein.

2. Design methodology

In Taguchi's method, the quality characteristics are usually divided into (1) nominal-is-best, (2) smaller-the-better, and (3) larger-the-better. The flow chart of a design of experiment for our case is shown in Fig. 1.

The magnitude of the optical transfer function (OTF), describing the spatial variation as a function of spatial frequency, is known as the modulation transfer function (MTF). MTF may be used to evaluate the imaging quality as well as the contrast issue in photography. The spatial frequency is expressed in lp/mm (line pairs per mm). Optical analysis stage is to determine the degree of reliance of the MTF; we make use of the optical software to determine the degree of coupling of MTF with some of the system/process parameters (control factors). At the stage of the construction of a simulation model, process parameters of the manufacturing system come into the view. Therefore, the set of control factors can be selected, and the number of levels for each control factor can be determined accordingly. The orthogonal array can be established. After the employment of software simulation, analysis through both signal-noise-ratio (S/N) and analysis of variance (ANOVA) is applicable. Optimal parametric combination of control factors with associated levels can be done by those dominant factors and levels summarized in the S/N and ANOVA tabulations.

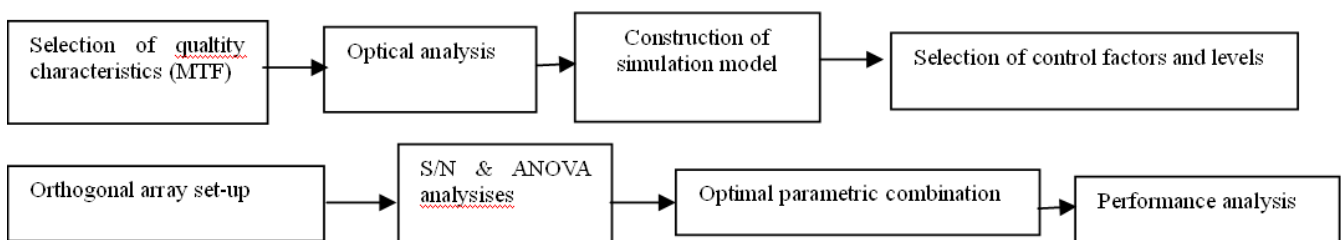


Fig. 1 The block diagram for the proposed scenario

Generally speaking, the performance of the quality characteristics can be evaluated through the three indices, defined by Taguchi, namely, the smaller-the-better (SB), the nominal-the-best (NB), and the larger-the-better (LB), all expressed in db;

$$\eta_{SB} = -10 \log \left\{ \frac{1}{n} \sum_{i=1}^n y_i^2 \right\} \quad (1)$$

$$\eta_{NB} = -10 \log \left\{ \frac{1}{n} \sum_{i=1}^n \frac{1}{y_i^2} \right\} \quad (2)$$

$$\eta_{LB} = 10 \log \left\{ \frac{\bar{y}}{S^2} \right\} \quad (3)$$

where

y_i : quality characteristics

\bar{y} : expectation of y

S^2 : sample variance.

3. Experiment

A prototype lens assembly with four aspherical lens mounted in a cascade manner is introduced for the experiment.[6-8] Assignments of lens' parameters are shown in Fig. 2, where R stands for radius while S means surface. Owing to the requirements of light weight and miniature size for optical lens, plastic material is employed.

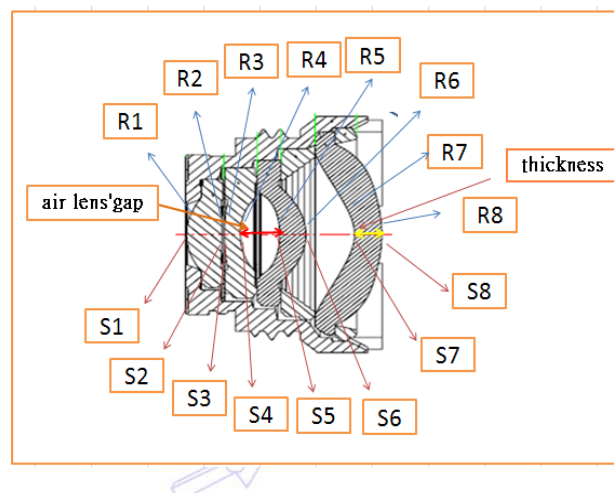


Fig. 2 The assignments of lens' numbers

Speaking of the MTF values selected for this paper, spherical aberration, coma and astigmatic will affect the sharpness of the image field curvature. Distortion will only result in a change of image position and shape had no effect on the resolution, which is incorrect aberration. Distortion and field curvature repair very good but let MTF values can not meet the requirements, because the aberration is not likely to be fully eliminated.

3.1. Sensitivity Analysis

We propose the use of optical software to accomplish the sensitivity analysis of lens manufacturing. Arbitrarily choosing MTF equal to 80 lp/mm along tangential direction (sampling at 0.5F, 0.7F, and 0.9F) and setting object location at infinity, we can easily visualize which control factor should be included in the degree of reliance (DOR) or sensitivity analysis. The results are tabulated in Table 1. Those highlighted grids are so significant for the sensitivity analysis, and are therefore recruited for analysis. For example, if the misplaced quantity is -0.003mm for L1R1 (radius of lens #1), the degradation of MTF will be ranged from 13% to 23% accordingly.

Table 1 Sensitivity analysis of MTF

| Ranking | Description | Tolerance | MTF | | |
|---------|--|-----------|------|------|------|
| | | | 0.5F | 0.7F | 0.9F |
| | | | 6 | 6 | 5 |
| 1 | L ₁ R ₁ misplaced | +0.003mm | 0% | 0% | -1% |
| | | -0.003mm | -13% | -20% | -23% |
| 2 | L ₁ R ₁ tilt & misplaced | +0.003mm | 0% | 0% | 0% |
| | | -0.003mm | -11% | -17% | -17% |
| 3 | L ₂ R ₂ misplaced | +0.003mm | -10% | -15% | -16% |
| | | -0.003mm | 0% | 0% | 0% |
| 4 | L ₂ R ₁ misplaced | +0.003mm | 0% | 0% | 0% |
| | | -0.003mm | -14% | -15% | -8% |
| 5 | L ₃ R ₁ misplaced | +0.003mm | 0% | 0% | -6% |
| | | -0.003mm | 0% | 0% | 0% |
| 6 | L ₁ thickness | +0.005mm | -1% | -1% | 2% |
| | | -0.005mm | 1% | 0% | -2% |
| 6 | L ₁ L ₂ air lens' gap | +0.005mm | -1% | -2% | -2% |
| | | -0.005mm | -1% | 1% | 1% |
| 6 | L ₂ L ₃ air lens' gap | +0.005mm | -1% | 1% | 2% |
| | | -0.005mm | 1% | -1% | -2% |
| 7 | L ₂ thickness | +0.005mm | 0% | 0% | 1% |
| | | -0.005mm | 0% | 0% | -1% |
| 7 | L ₃ thickness | +0.005mm | 0% | 0% | 1% |
| | | -0.005mm | 0% | 0% | -1% |
| 7 | L ₃ L ₄ air lens' gap | +0.005mm | 0% | 1% | 1% |
| | | -0.005mm | 0% | -1% | -1% |

3.2. Analytical Model

Table 2 The feasible process parameters in manufacturing system

| L ₁ | specification | measured | L ₂ | specification | Measured |
|---|---------------|----------|---|---------------|----------|
| Outer diameter | ∅2.9±0.005 | 2.911 | Outer diameter | ∅3.5±0.005 | 3.511 |
| thickness | 0.75±0.005 | 0.753 | thickness | 0.33±0.005 | 0.336 |
| Air lens' gap (L ₁ -L ₂) | 0.05±0.005 | 0.061 | Air lens' gap (L ₂ -L ₃) | 0.83±0.005 | 0.8205 |
| S ₁ absolute | 0-0.003 | 0.00545 | S ₃ absolute | 0-0.003 | 0.01028 |
| S ₂ absolute | 0-0.003 | 0.00528 | S ₄ absolute | 0+0.003 | 0.00227 |
| Total | 0±0.003 | 0.00143 | Total | 0±0.003 | 0.01219 |
| Best R1 -X | N/A | 1.6003 | Best R3 -X | N/A | 9.9967 |
| Best R1 -Y | N/A | 1.6 | Best R3 -Y | N/A | 10.035 |
| Best R2 -X | N/A | -7.475 | Best R4 -X | N/A | 1.90401 |
| Best R2 -Y | N/A | -7.45 | Best R4 -Y | N/A | 1.904802 |
| L ₃ | Specification | Measured | L ₄ | specification | Measured |
| Outer diameter | ∅3.9±0.005 | 3.904 | Outer diameter | ∅5.4±0.005 | 5.397 |
| thickness | 0.55±0.003 | 0.552 | thickness | 0.57±0.005 | 0.571 |
| Air lens' gap (L ₃ -L ₄) | 1.021±0.005 | 1.0205 | Air lens' gap (L ₄ -) | N/A | N/A |
| S ₅ absolute | 0±0.003 | 0.0024 | S ₇ absolute | 0±0.003 | 0.0078 |
| S ₆ absolute | 0±0.003 | 0.0093 | S ₈ absolute | 0±0.003 | 0.0015 |
| Total | 0±0.003 | 0.0080 | Total | 0±0.003 | 0.0093 |
| Best R5 -X | N/A | -2.5430 | Best R7 -X | N/A | -1.2500 |
| Best R5 -Y | N/A | -2.5430 | Best R7 -Y | N/A | -1.2493 |
| Best R6 -X | N/A | -1.4995 | Best R8 -X | N/A | -3.4910 |
| Best R6 -Y | N/A | -1.4989 | Best R8 -Y | N/A | -3.4900 |

Experiment is performed after the sensitivity analysis with the help via optical software. Uncontrollable and unexpected consequences associated with selected factors may come to the view when the output dataset from optical software analysis is directed to the manufacturing phase. In order to simulate the lens' manufacturing process as close as possible to the actual scenario, we establish a process parameters-directed, analytical simulation model. By referring to the actual experimental results, those factors having substantial degree of significance related to the MTF are back substituted to the optical software to improve the quality characteristics. The manufacturing capability is characterized through the numeric summarized in Table 2 with all units in mm. The factors associated with the process parameters to be used in the manufacturing stage are thickness (L1 to L4), eccentricity (lateral offset and tilt), surface profile (best R value), and the air lens' gaps.

3.3. Orthogonal Array Selection

The relationship between lens' optical parameters and actual manufacture tolerance for each lens' component is investigated. Our design philosophy is to wisely pick up those control factors/parameters. A variety of test-beds is making our experiment scenario complicated.[9-11] For simplicity, the default values for the experiment issue are – finite location to infinity for object, spatial frequency set to 120 lp/mm, and the outputs are MTF values along tangential direction. The MTF test point locations are illustrated in Fig. 3. Those three concentric circles are the locations for 50%, 70%, and 100% of image heights.

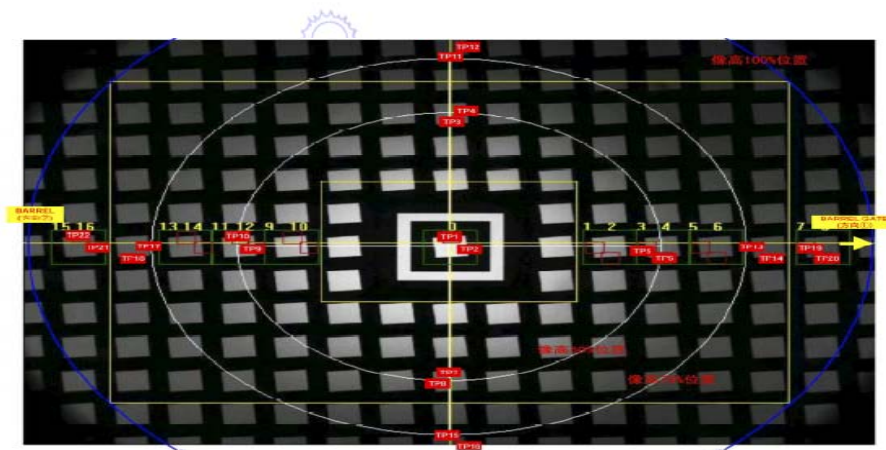


Fig. 3 Illustration of MTF sampling locations

There are eight control factors in our experiment, and the number of experiments to be conducted is 6561 with three levels for each control factor. Alternatively, a L18 orthogonal array is adopted to reduce the number of experiments down to 18, provided that one of these control factor's levels needs to be adjusted to 2. We arbitrarily choose the first control factor, the air gap between lens #1 and lens #2. A complete list of control factors and their associated levels is in Table 3, and the L18 orthogonal array is referred to Table 4. Noticed that the level 3 of control factor "A" is intentionally neglected due to the use of L18 array instead of L27(313) array.

Table 3 List of the control factors and associated levels

| Control factor | Description | Default value(mm) | Level 1(mm) | Level 2(mm) | Level 3(mm) |
|----------------|-----------------------------|-------------------|-------------|-------------|-------------|
| A | Air gap (L1 – L2) | 0.55 | 0.045 | 0.05 | 0.047 |
| B | Air gap (L2 – L3) | 0.83 | 0.825 | 0.83 | 0.835 |
| C | Air gap (L3 – L4) | 1.021 | 1.024 | 1.021 | 1.026 |
| D | L ₂ eccentricity | 0 | -0.005 | 0 | 0.003 |
| E | L ₃ eccentricity | 0 | -0.005 | 0 | 0.003 |
| F | L ₄ eccentricity | 0 | -0.005 | 0 | 0.003 |
| G | L ₂ thickness | 0.33 | 0.33 | 0.33 | 0.335 |
| H | L ₃ thickness | 0.55 | 0.553 | 0.55 | 0.555 |

Table 4 Simulation using L18 orthogonal array and its corresponding MTF and signal-to-noise ratios

| Exp | A | B | C | D | E | F | G | H | MTF value | S/N |
|-----|---|---|---|---|---|---|---|---|-----------|---------|
| 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0.6100 | -4.2934 |
| 2 | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 0.5900 | -4.5830 |
| 3 | 1 | 1 | 3 | 3 | 3 | 3 | 3 | 3 | 0.5000 | -6.0206 |
| 4 | 1 | 2 | 1 | 1 | 2 | 2 | 3 | 3 | 0.5700 | -4.8825 |
| 5 | 1 | 2 | 2 | 2 | 3 | 3 | 1 | 1 | 0.6400 | -3.8764 |
| 6 | 1 | 2 | 3 | 3 | 1 | 1 | 2 | 2 | 0.5400 | -5.3521 |
| 7 | 1 | 3 | 1 | 2 | 1 | 3 | 2 | 3 | 0.7400 | -2.6154 |
| 8 | 1 | 3 | 2 | 3 | 2 | 1 | 3 | 1 | 0.5100 | -5.8486 |
| 9 | 1 | 3 | 3 | 1 | 3 | 2 | 1 | 2 | 0.5700 | -4.8825 |
| 10 | 2 | 1 | 1 | 3 | 3 | 2 | 2 | 1 | 0.4600 | -6.7448 |
| 11 | 2 | 1 | 2 | 1 | 1 | 3 | 3 | 2 | 0.5900 | -4.5830 |
| 12 | 2 | 1 | 3 | 2 | 2 | 1 | 1 | 3 | 0.6400 | -3.8764 |
| 13 | 2 | 2 | 1 | 2 | 3 | 1 | 3 | 2 | 0.6400 | -3.8764 |
| 14 | 2 | 2 | 2 | 3 | 1 | 2 | 1 | 3 | 0.5500 | -5.1927 |
| 15 | 2 | 2 | 3 | 1 | 2 | 3 | 2 | 1 | 0.5700 | -4.8825 |
| 16 | 2 | 3 | 1 | 3 | 2 | 3 | 1 | 2 | 0.5200 | -5.6799 |
| 17 | 2 | 3 | 2 | 1 | 3 | 1 | 2 | 3 | 0.5800 | -4.7314 |
| 18 | 2 | 3 | 3 | 2 | 1 | 2 | 3 | 1 | 0.7200 | -2.8534 |

After substituting the listed parameters shown in Table 3 and Table 4 and the entries in the orthogonal array L18(21×37) into optical software, the corresponding MTF values and their computed S/N ratios are listed in Table 4. The quality characteristics chosen is the MTF, and the selected S/N ratio is the larger-the-better. It is expressed as

$$(S/N)_{\text{larger-the-better}} = -10 \log \left(\frac{1}{n} \sum_{i=1}^n \frac{1}{\text{MTF}_i^2} \right) \quad (4)$$

where n is the number of experiments being conducted. The impact of S/N versus control factors with designated levels is drawn in Fig.4. The impact of quality characteristics, MTF, versus control factors is shown in Fig.5. ANOVA is therefore performed to confirm the significances of those selected control factors, based on the setting of 95% confidence interval; the results are illustrated in Table 5. The degree of significance is marked by either “yes” or “no.”

The degree of contribution of variance can be visualized via the column termed “F,” the F-ratio test. The ranking is as follow — D, E, and B. The contribution of the optical system up to the greatest impact, which control factor D, confidence of the highest 100% probability that can enhance the quality characteristics, followed by control factor E, respectively, 99.5% probability, 96.8% probability.

Table 5 The ANOVA results

| Factor | SS | DOF | Var | F | Confidence | Significant?* |
|--------|--------|-----|--------------------------|-------|------------|---------------|
| A | 0.00 | 1 | 0.00 | 0.0 | 4.9% | No |
| B | 1.02 | 2 | 0.51 | 9.2 | 96.8% | Yes |
| C | 0.08 | 2 | 0.04 | 0.7 | 46.4% | No |
| D | 14.43 | 2 | 7.21 | 129.2 | 100.0% | Yes |
| E | 2.85 | 2 | 1.42 | 25.5 | 99.5% | Yes |
| F | 0.20 | 2 | 0.10 | 1.8 | 72.5% | No |
| G | 0.11 | 2 | 0.06 | 1.0 | 55.6% | No |
| H | 0.24 | 2 | 0.12 | 2.1 | 76.6% | No |
| Others | Pooled | | | | | |
| Error | 0.22 | 4 | 0.06 | | | |
| Total | 18.96 | 17 | *At least 95% confidence | | | |

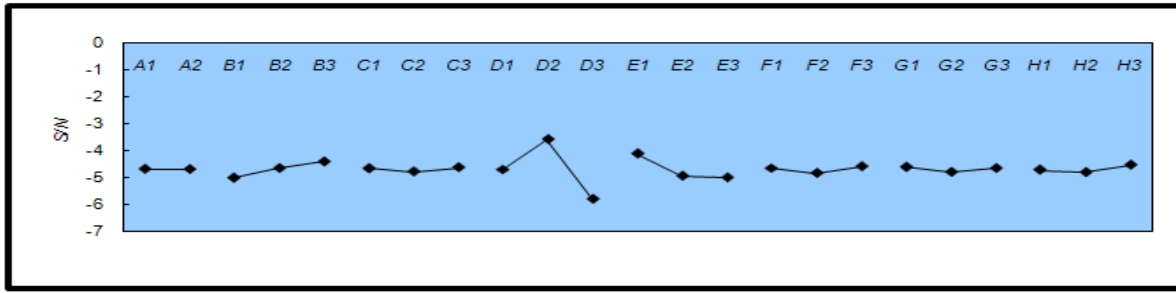


Fig. 4 The impact of S/N versus control factors

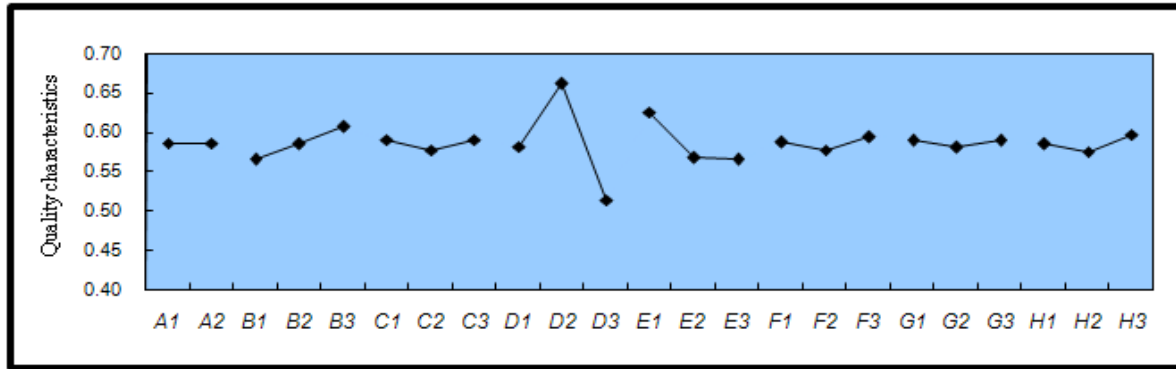


Fig. 5 The impact of quality characteristics, MTF, versus control factors

3.4. Optimal Parameters Combination

In summary, we perform the optical analysis via software, the impacts of MTF with various control factors with levels, and finally the ANOVA. The optimal combination/selection of control parameters becomes obvious. Initially, the decision is made, and the optimal parameter set is {B3, D2, E1}. The degree-of-reliance (DOR) to the quality characteristics is further categorized into three classes. The optimal parametric combination is therefore sought. For the purpose of analysis, Table 6 shows the classification of the control factors. In Table 6, Q.C. stands for quality characteristics. By adjusting the factors in class #1 to maximize the S/N, we obtain the following combination, A*-B3-C*-D2-E1-F*-G*-H*, where (*) stands for that user can select any of the corresponding levels (1-3); those factors belonging to class #2 are tuned next. Finally, the ultimate optimal combination is A1(orA2)-B3-C3-D2-E1-F3-G1-H3. The response curves of MTF before and after the introduction of Taguchi design are plotted in Fig.7 and Fig.8, illustrating the increasing of MTF values from 55.6% to 60% at the spatial frequency of 120 lp/mm. The preceding analysis and the choosing of optimal control factors with assigned level are directed to the lens manufacturing. The manufactured high-resolution camera/cell-phone lenses are included in Fig.6. Multiple performance characteristics (MPC) may be recruited to have further improvement in lens manufacturing issue, but the design complexity and the computational load will be increased tremendously. The improvement of S/N comparing to the original default/design specs, choosing {B3, D2, E1}, is

$$\nabla(S/N) = 0.02 + 0.06 = 0.08.$$

(5)

where $\nabla()$ stands for difference operation. Actually, the increment of S/N value confirms the effort in seeking the optimal combination of control factors.

Table 6 Classification of control factors

| class | Coupled with S/N | Coupled with Q.C. | Control Factor | Purpose |
|-------|------------------|-------------------|----------------|------------------------|
| 1 | Yes | Yes/No | B,D,E | Variation minimization |
| 2 | No | Yes | C,F,G,H | Desired Q.C. |
| 3 | No | No | A | Cost reduction |



Fig. 6 The manufactured high-resolution camera/cell-phone lenses using the Taguchi design

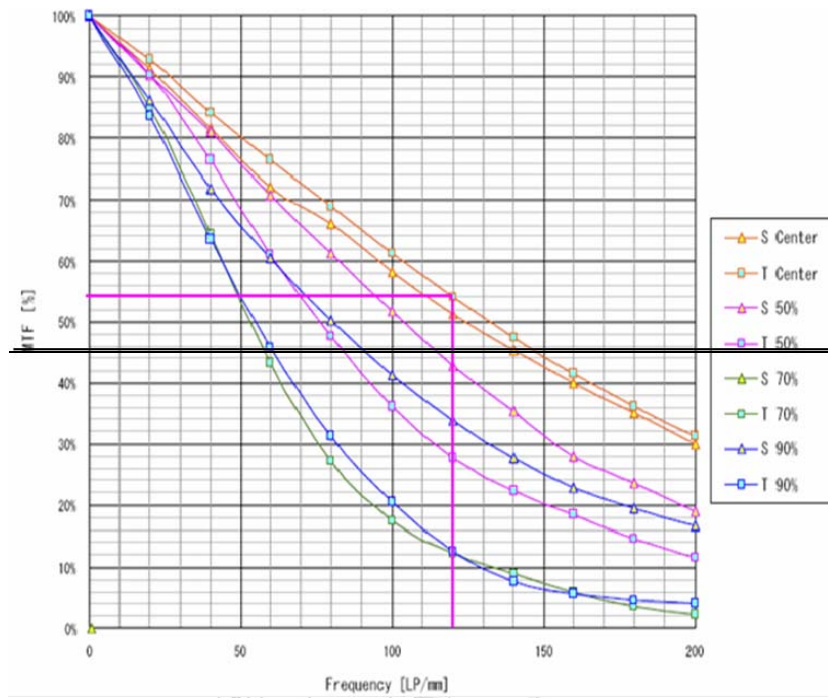


Fig. 7 The impact of MTF vs. frequency before the introduction of Taguchi method (S:Sagittal, T:Tangential)

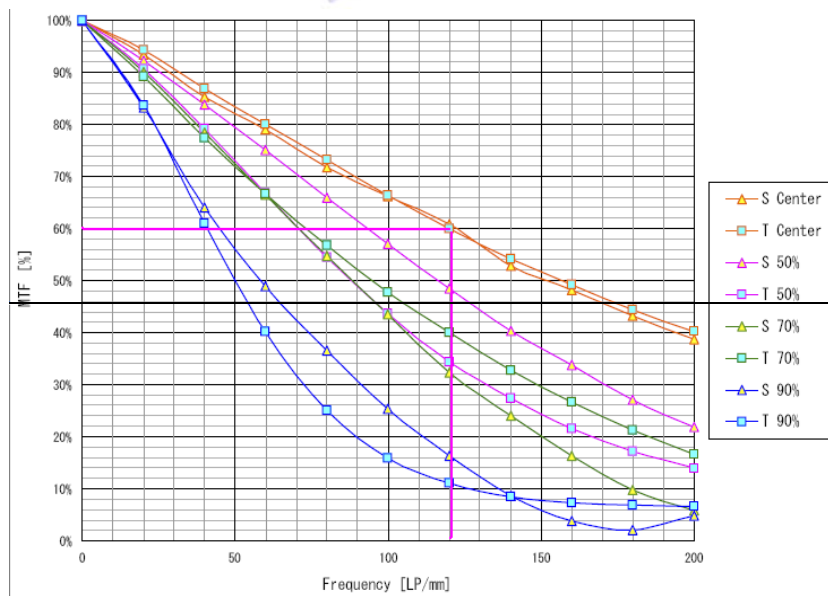


Fig. 8 The impact of MTF vs. frequency after the introduction of Taguchi method (S:Sagittal, T:Tangential)

4. Conclusions

An effort to promote the image quality via the increasing of the value of modulation transfer function throughout the generic two-stage design has been proposed and verified through software simulation with two key features, signal-to-noise ratio and the analysis of variance, and may finally be directed to mass production process. With the help from the analysis using optical software, a simulation model is constructed and incorporated with Taguchi's method to fulfill the ultimate goal, i.e., cost reduction and shortening developmental or enter-to-market time; meanwhile, the optimal/suboptimal combination of the process parameters is obtained. Those most significant control factors relating to the quality characteristics, MTF, are analyzed. The comparisons of responses (MTF) between the manufactured and the designed are conducted. Those crucial control factors chosen are very common in lens manufacturing industries. Instead of employing trial-and-error strategy to promote the quality of high resolution lens, the proposed analysis combining Taguchi method with analysis of variance is, for sure, simple, practical, and applicable in a variety of applications. It also provides a guideline to the manufacturing of miniature lens, exclusively with the manufacturing capability-oriented design criteria in a manufacturing process.

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